

Properties and Applications of Thick Film High Temperature Superconductors

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Abstract—Melt processed $\text{YBa}_2\text{Cu}_3\text{O}_x$ thick films display low surface resistance, moderate performance in fields and can be applied to three-dimensional (3-D) substrates with ease. The processing and properties of such films are described. Possible applications are examined and prototype devices are described. These include high Q , low frequency resonators for cellular communications filters, low phase noise oscillators, magnetic resonance imaging receiver coils, low noise magnetic shields, coils, flux transformers, and antennas.

I. INTRODUCTION

FOR SOME applications of high temperature superconductor (HTS) films it would be advantageous for the HTS layer to be applied over large areas and curved surfaces. Such applications include high Q resonators, antennas, large magnetic resonance imaging (MRI) receiver coils, magnetic shields, coils, and certain flux transformer designs. HTS thin films may be unsuitable if not impossible to manufacture in many of the geometries required and HTS thick films, which can be applied to curved surfaces and over large areas, offer a viable alternative. Such films can have a current density of around 2000 A cm^{-2} at 77 K , possess a far better resistance to magnetic fields than bulk sintered HTS, and have a surface resistance, R_s , of approximately $2 \text{ m}\Omega$ (10 GHz and 77 K). In this paper we examine possible applications where thick film $\text{YBa}_2\text{Cu}_3\text{O}_x$ (YBCO) could demonstrate a significant improvement over other materials. Particular emphasis is placed on the RF and microwave applications although mention is also made of some of the important magnetic and dc applications.

II. FABRICATION

All the devices described in this paper were made by thick film methods [1], [2], involving depositing $\text{YBa}_2\text{Cu}_3\text{O}_7$ on to a 3 mol % yttria stabilized zirconia substrate. First, the superconducting powder was made by mixing BaCO_3 , CuO , and Y_2O_3 together and heating to $\sim 900^\circ\text{C}$ and then grinding the

Manuscript received February 28, 1996; revised March 19, 1996. This work was supported by the U.K. Department of Trade and Industry and Defence Research Agency, the U.S. Department of Commerce, and the HTSSE Programme.

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Publisher Item Identifier S 0018-9480(96)04799-0.

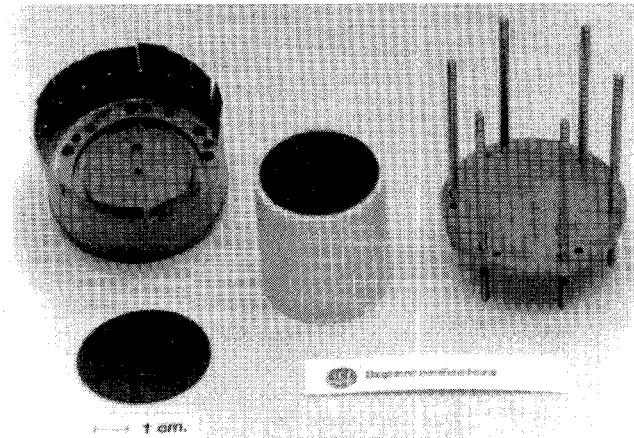


Fig. 1. 10 GHz YBCO thick film cavity (dismantled).

mixture to a fine powder. The powder was made into a thick ink by mixing with polymers and solvents on a three roll mill. The ink was then deposited onto the zirconia substrate—which could be in the form of wires, coils, tubes, or plates—by screen printing or doctor blading. The coated substrates were then sintered in an oxygen atmosphere at temperatures of around 1000 – 1050°C . Zirconia substrates were chosen because of their high strength ($\sim 800 \text{ MPa}$) and toughness ($6 \text{ MPam}^{1/2}$). Tolerance to shock and vibration is excellent thus avoiding a key concern with regard to some applications. Although there is a reaction between the substrate and the superconductor which forms mainly barium zirconate this reaction layer does not impair the superconducting properties and does in fact provide an excellent adhesive bond. After firing the thick film body was masked and patterned as necessary.

III. PROPERTIES AND APPLICATIONS

A. High Q TE_{011} Cavities

At 77 K thick film YBCO has a surface resistance less than copper for frequencies $\leq 50 \text{ GHz}$ [1], and thus the use of the HTS material can be advantageous in certain RF and microwave applications. Thick film YBCO cavity resonators operating in the TE_{011} mode have been constructed. A cavity resonating at 5.66 GHz had an unloaded Q of 715 000 at 77 K , which corresponds to $R_s = 1.09 \text{ m}\Omega$ [3]. A 10 GHz cavity has been made to form part of the local oscillator circuit of a cryogenic downconverter system in a collaborative project supported by the U.K. Department of Trade and Industry. The

TABLE I
PHASE NOISE OF 7.5 GHz OSCILLATORS

| Oscillator System | Measurement Temperature (K) | Phase Noise (dB Hz^{-1}) | |
|-------------------|-----------------------------------|------------------------------------|--------------|
| | | 1kHz offset | 10kHz offset |
| Cu Cavity | 300 | -90 | -120 |
| Cu Cavity | 77 | -95 | -124 |
| HTS Cavity | 77 | -108 | -135 |

cavity is shown in Fig. 1. Unloaded Q values of over 10⁵ have been measured for the cavity at 77 K, and the complete oscillator, which also incorporates a GaAs HEMT, had phase noise values of -94 and -120 dB Hz^{-1} at 10 kHz and 100 kHz offsets, respectively, from the carrier frequency [4].

Improvements in close-to-carrier noise of a simple 7.5 GHz oscillator incorporating a thick film HTS resonator have also been measured. The oscillator circuit consisted of an GaAs MESFET amplifier, 3 dB feedback power splitter, a variable attenuator, and a phase shifter with either a TE₀₁₁ mode copper cavity or a high Q , HTS thick film replacement. The TE₀₁₁ cavities each comprised a cylindrical barrel and a pair of closing end plates. Unloaded Q factors (Q_0) for the copper and YBCO cavities were measured to be 65 000 and 500 000, respectively, at 77 K. At a lower temperature of 64 K, Q_0 of the YBCO cavity increased to over 10⁶, indicating that the R_s of the YBCO was reduced by a factor of 2. Phase noise measurements were carried out with the entire oscillator circuit at the measurement temperature, either 300 or 77 K, and are summarized in Table I. It should be noted that these phase noise measurements were limited by the noise floor of the measurement system, but the results demonstrate the potential use of high Q HTS resonators in low phase noise systems.

The surface resistance of the thick film materials has been measured at a number of frequencies in the range 5–50 GHz [1], [3]–[5]. In general, these measurements have been made using TE_{01n} cavities constructed either wholly or partly of YBCO thick film elements. The dependence of R_s on frequency is shown in Fig. 2 and demonstrates that the surface resistance exhibits an approximately squared dependence. For comparison, typical data from epitaxial thin films and bulk YBCO are also plotted on Fig. 2.

B. Lower Frequency Resonators

For lower frequency applications, around 1 GHz, the TE₀₁₁ resonator is not a convenient size to cool, and certainly a series of such resonators constructed to make a filter would not be practical. One alternative geometry would be to use HTS coaxial elements with either a normal metal or HTS outer shield. We have manufactured these and other electrically small, three-dimensional (3-D) resonant structures from thick film YBCO and measured Q values over 86 000. Filters

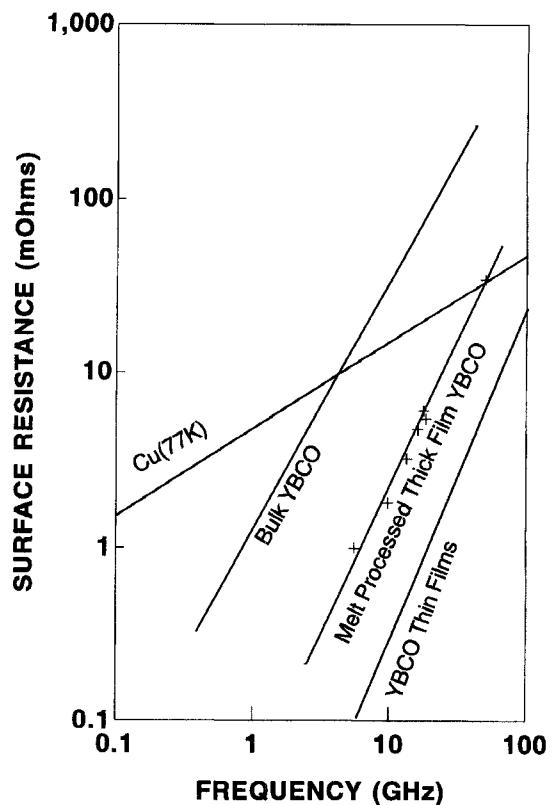


Fig. 2. Frequency dependence of surface resistance for YBCO thick films, bulk materials, and thin films.

constructed from such resonators demonstrate low insertion loss and good rejection characteristics [6]. A key performance requirement in this application is a low dependence of Q on RF power which can cause nonlinearities in the device and can drastically affect the intermodulation performance [7]. The RF power dependence and excellent intermodulation performance for the thick film materials are shown in Figs. 3 and 4, respectively. Filters incorporating similar thick film resonant elements are currently undergoing field trials.

C. Antennas and MRI Components

Planar antennas [8] and superdirective arrays [9] operating at less than 1 GHz have been demonstrated in thick films. The

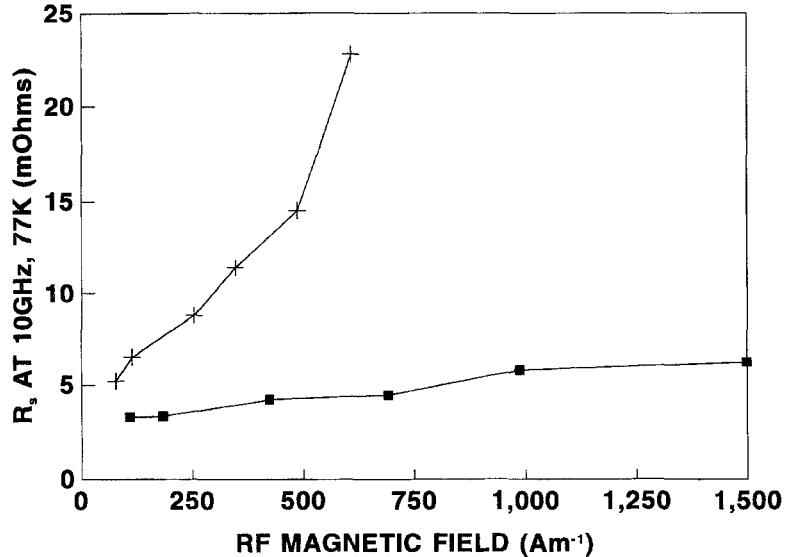


Fig. 3. RF power dependence of standard YBCO (+) and improved melt processed thick films (■).

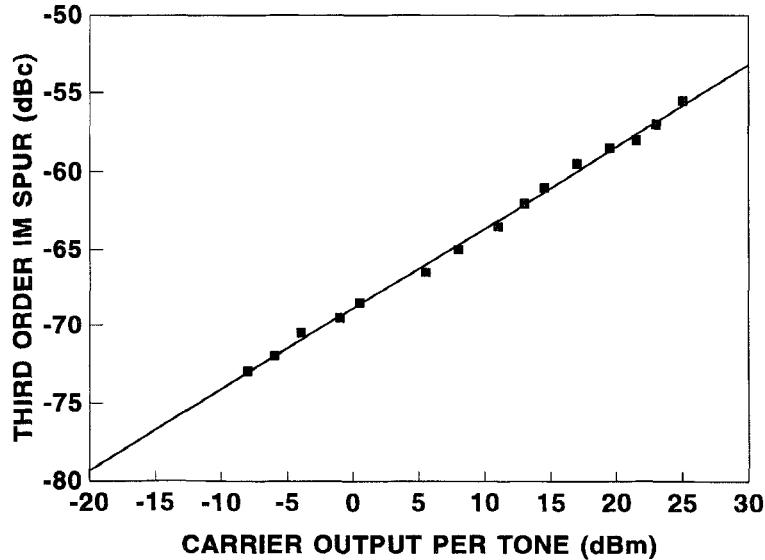


Fig. 4. Intermodulation performance of 16-pole GSM receive filter incorporating YBCO thick film elements, measured at 77 K.

reduced loss in the superconductor means that the antenna may be made electrically small without a drastic loss in efficiency. At 500 MHz, a gain of around 6 dB is measured at 77 K for loop and dipole antennas in comparison with copper counterparts. It should be noted that for this application the construction of the matching networks also used thick film HTS. Antenna arrays incorporating patterned HTS thick films on both sides of a 4" \times 4" substrate are shown in Fig. 5.

An example of a large area, low frequency coil is a receiver coil used in MRI. The use of HTS coils as receiver coils was first suggested by Hall *et al.* [10] who showed an improvement in the signal-to-noise ratio (SNR) of a coil for use in a field of 0.15 T (6.67 MHz). For this application there are two main sources of noise. Coil noise which is influenced by its resistance, and body noise which is due to the electrical conductivity of the body. The body noise increases with frequency, so that if measurements are made at low frequency,

i.e., low field, with the correct geometry, the coil noise can be made to dominate. The noise power due to the coil is proportional to $4 kT R$, where T is temperature and R is the resistance of the coil. Therefore to reduce the noise, the resistance, temperature or both must be reduced. It should be noted that for ac signals the resistance of the superconductor is not zero but is far less than the resistance of normal metals at the low frequencies used for MRI. We also note that as well as increasing the SNR, the use of a HTS coil also increases the Q as $Q = \omega L/R$, so that reducing R also increases sensitivity. Various designs of HTS thick film MRI receiver coils are currently being examined.

D. Magnetic Properties and Applications

HTS thick film materials can also prove useful in non-RF applications. Superconductors are perfect diamagnetic shields.

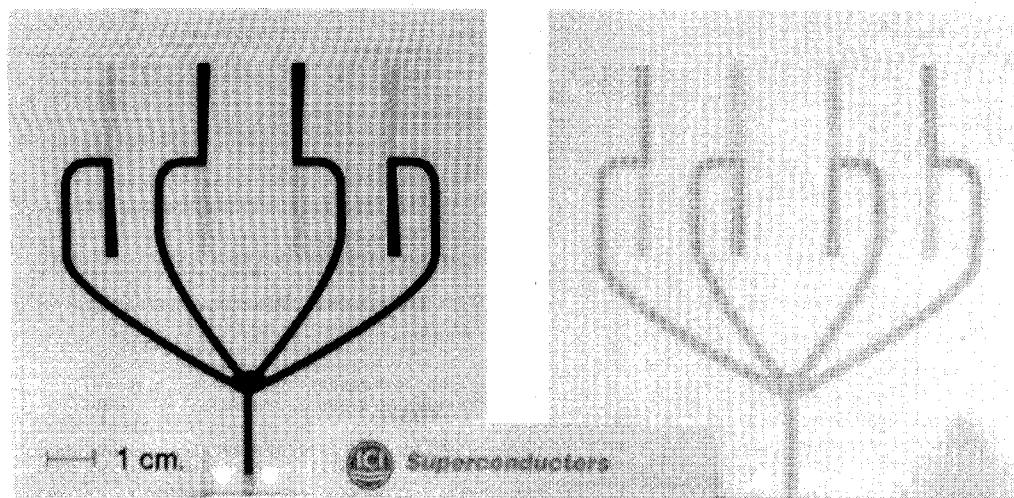


Fig. 5. Antenna arrays on 4" x 4" double-sided YBCO thick film substrates.

There are three main issues regarding shields. The first is shielding out background noise and the earth's field. The earth's field is approximately 0.05 mT and there is little problem in constructing thick film shields capable of this level of screening. In fact, the shields made by thick film methods will screen between 0.5 to 1 mT at 77 K [11]. The second is the issue of flux creep and here the behavior of thick film shields has been investigated by Muirhead *et al.* [12] who found that the current density of the shields was of the order 600 A cm^{-2} . For a shielded area of a square centimeter, a creep rate of 10^{-5} flux quanta per second can be shown to correspond to $2 \times 10^{-20} \text{ V}$ and, at the lowest voltages, the measurements suggest that the flux creep is adequately low for shield applications. The third issue is the manufacturing route and choice of material. The flux creep performance of YBCO has been demonstrated to be superior to that of BSCCO in our experiments and the method of application onto zirconia substrates appears highly successful. Coatings can be applied to both inside and outside surfaces thereby increasing the performance of the shields.

Exceptionally low noise is required for certain applications where $1/f$ noise and stochastic variation of flux pose problems. In a SQUID, for example, it is clearly important to determine the flux noise in both the thin film component and the screening system ie the shield. The noise properties of YBCO-SrTiO₃-YBCO thin film multi-loop magnetometers enclosed within YBCO thick film shields has been measured at 77 K by Ludwig *et al* [13] and found to be very low at $37 \text{ fTHz}^{-1/2}$ and $18 \text{ fTHz}^{-1/2}$ at 1 Hz and 1 kHz respectively.

Flux transformers and gradiometers have been manufactured using thick film processing techniques and results on both planar and 3-D structures are encouraging. A planar flux transformer consisting of two loops trapped a flux of 25 mG. In an analysis of the creep behavior it was determined that the device worked well down to 10 mHz with a circulating current of 45 mA. Tests at 25 mA, representing a field of $1.5 \mu\text{T}$, demonstrated that the device was adequate for most applications. Crossunders using through-substrate vias have also been demonstrated in both planar and 3-D geometries.

IV. CONCLUSION

The manufacture of high quality thick film artefacts has been described, and several useful devices have been demonstrated. The properties of epitaxial thin film materials will always be potentially superior to those of polycrystalline thick films. However, the main advantages of the thick film materials result from the ability to produce 3-D and large area structures with properties which are more than adequate for many applications. These type of structures cannot be made by thin film techniques.

Thick film resonators have been shown to possess high Q factors, low phase noise, excellent intermodulation performance and reasonable RF power dependence. Thick film shields were seen to have extremely low flux noise characteristics, also useful for the thick film flux transformers and gradiometers. The flux transformers and gradiometers were found to work well down to 10 mHz. Large area, low frequency antennas have been manufactured including MRI receiver coils. The outlook for the application of HTS thick film materials in areas exploiting their large area or 3-D capabilities is encouraging, and cellular communication filters incorporating this technology are already in production.

ACKNOWLEDGMENT

The authors would like to thank their colleagues at the University of Birmingham, U.C. Berkeley, and GEC-Marconi, and A. Abdelmonem, M. Beik, and R. Lithgow of the Illinois Superconductor Corporation.

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of prototype components

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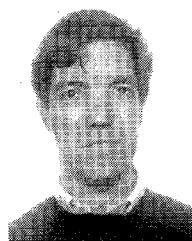
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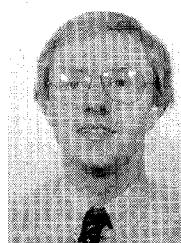
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Neil M. Alford was a Divisional Research Associate with ICI from 1981 to 1994. He was responsible for the superconductivity effort at ICI which resulted in the first HTS antenna, the first HTS generator and the lowest surface resistance thick film HTS material measured at microwave frequencies. He is now Professor of Physical Electronics and Materials at South Bank University, London, U.K., and leads a team examining superconductivity and dielectric materials.